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BEC/allwaste Field Trial of of FPC-1 Fuel Performance Catalyst

Test conducted for BEC/allwaste by UHI Corporation Provo, Utah and FPC Limited Houston, Texas

September 15, 1996

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Abstract

This paper discusses the results of a field test conducted by BEC/allwaste, Birmingham, Alabama, to determine the economic and environmental benefits from fuel treatment with a unique combustion catalyst called FPC-1. The study was planned in cooperation with and approved by Mr. Frank Montgomery, Equipment Coordinator. The test was conducted by Mr. Mike Cencula, Purchasing Coordinator for BEC/allwaste, Mr. Craig Flinders, VP Tech Services for UHI Corporation, and Messrs. Mark Newman and David Doctor of FPC Limited. The study conducted on a fleet of Cat and Cummins powered trucks and front loaders concluded the following:

- (1) All engines realized reductions in fuel consumption after FPC-1 fuel treatment. The fleet averaged a 11.63% reduction in fuel consumption.
- (2) FPC-1 treated fuel combusted more completely than the standard diesel. Unburned hydrocarbons (measured as n-hexane) were reduced 22.2%.
- (3) Smoke density was reduced 23.9% after FPC-1 fuel treatment.

These results verify substantial <u>fuel cost savings and environmental benefits</u> can be derived from FPC-1 use throughout the entire BEC/allwaste fleet operation. Along with the obvious fuel cost savings, maintenance cost reductions are inevitable with FPC fuel treatment. Smoke is simply soot, which is comprised of unburned fuel droplets. It is soot that builds up on critical engine components (injectors, valves, rings, seats, pistons, etc.) reducing engine efficiency and accelerating wear. That very fact that FPC reduces visible smoke attests to it's ability to prevent hard carbon (hardened soot) upon these critical engine components.

Motor oil will also stay carbon (soot) free longer, and thus maintain designed viscosity between oil changes. In this manner, abrasion wear of bearings, liners and rings is reduced.

The paper also discusses a unique, recognized test method for determining the benefits of FPC-1 in the field. The method is known as the carbon mass balance, which is central to the EPA standardized Federal Test Procedures and Highway Fuel Economy Test. The method uses exhaust gas analysis under steady-state engine operation to determine both fuel consumption and exhaust emissions.

I. Introduction

FPC-1 Fuel Performance Catalyst is a burn rate modifier or catalyst, proven to reduce fuel consumption and increase engine horsepower in several recognized, independent laboratory tests, and dozens of independent field trials. The catalyst also has a remarkable impact upon the products of incomplete combustion that are regulated by emissions reduction legislation (smoke and carbon monoxide).

The intent of the trial by BEC/allwaste was to determine the degree of fuel consumption, and emissions reduction resulting from the addition of the FPC-1 catalyst to the blended diesel fueling a select fleet of compression-ignition engine powered buses. The test methodology for determining fuel consumption is the carbon mass balance (cmb). The cmb method measures the carbon containing products of the combustion process (CO2, CO, HC) found in the exhaust, rather than directly measuring fuel flow into the engine. Also, while conducting the cmb procedure, a Bacharach Smoke Spot method is used to determine smoke density in the exhaust of the diesel powered equipment.

This report summarizes the results of baseline and FPC-1 treated fuel consumption and emissions data, and computes and compares the mass flow rates (engine performance factors or PFs) for the same.

II. Discussion of Carbon Mass Balance Method

The carbon mass balance eliminates virtually all of the variables associated with field testing for fuel consumption changes. The method requires no modifications to fuel lines or engines, and can be conducted in a short period of time at minimal expense.

Instead of measuring fuel flow into the engine (ie., the weight or volume of the fuel), measurements are made of the exhaust gases leaving the engine. More precisely, the carbon containing gases in the exhaust are measured. The method is based upon the Law of Conservation of Matter, which states that atoms can neither be created nor destroyed. Since the engines only source of carbon is the fuel it consumes, the carbon measured in the exhaust must come from the fuel. By measuring the carbon going out of the engine in the form of products of combustion, the amount of carbon entering the engine can be determined.

Carbon Balance Calculation

The carbon leaving the engine is mainly in the form of carbon dioxide (CO2), carbon monoxide (CO), unburned hydrocarbons (HC), and particulate (smoke). By collecting this data while the engine is operating at a given load and speed, the fuel flow rate into the engine can be accurately determined. When engine load and speed, along with other factors influencing fuel consumption are reproduced and/or monitored to make appropriate corrections, the carbon balance can be used to confidently determine changes in fuel consumption that might result from the use of a fuel catalyst, such as FPC-1.

With the carbon balance, engine efficiency is expressed in terms of engine performance factors. To calculate any change in engine performance, separate measurements are made with the engine running on base fuel (untreated) and FPC-1 treated fuel. Any changes are stated as percentage changes from the baseline.

A copy of the carbon balance equations is found on Figure 1 (Appendix 5). A sample calculation for illustration purposes is also attached (see Figure 2, Appendix 5). Additionally, the carbon balance can be used to determine the effect of FPC-1 upon harmful emissions, such as carbon monoxide and smoke.

III. Instrumentation

Precision, state-of-the-art instrumentation is used to measure the concentrations of carbon containing gases in the exhaust stream and other factors related to fuel consumption and engine performance. The instruments and their purposes are listed below:

- 1) A Sun Electric SGA-9000 non-dispersive infrared (NDIR) four gas analyzer measures the volume percent of CO2, CO, and oxygen (O2) in the exhaust, and the parts per million (ppm) of HC.
- 2) EPA I/M Calibration Gases known gases used internally to calibrate the NDIR analyzer.
- 3) A twenty (20) foot sampling train and stainless steel exhaust gas probe inserted into the engine exhaust pipe and used to draw a sample of exhaust gases to the analyzer.
- 4) A Fluke Model 52 hand held digital thermometer and wet/dry thermocouple probe measures exhaust, ambient, and fuel temperature.
- 5) A Dwyer Magnehelic 2000 Series Pressure Gauge and pitot tube measures exhaust air velocity and/or pressure.
- 6) A Monarch Contact/Noncontact digital tachometer and magnetic tape measures engine rpm when dash mounted tachometers are unavailable.
 - 7) A hydrometer and flask determines fuel specific gravity (density).
 - 8) Barometric pressure is acquired from local airport or weather station.
 - 9) A Bacharach Truespot Smokemeter for smoke density determination.

Except for engine speed, fuel density, and ambient readings, all data are collected by simply inserting probes into the exhaust stream while the engine is running at a fixed rpm and load, and the vehicle is stationary. No modifications or device installations are made to the fuel system,

nor are normal equipment work cycles disrupted.

IV. Technical Approach

The following technical approach was observed during both test segments:

- 1) All instruments are calibrated according to accepted protocol.
- 2) A sample of fuel is drawn from the fuel tank on each piece of equipment. Using a hydrometer and wet/dry temperature probe, fuel specific gravity and temperature are recorded.
- 3) Each piece of equipment to be tested is parked, brakes locked, and run out-of-gear at a specific engine speed (RPM) until engine water, oil, and exhaust temperature, and exhaust pressure have stabilized. Engine speed is controlled using either a hand held phototach, or the tachometer in the cab, and either a Snap-On throttle lock, a high idle switch, or the programmable computer onboard the truck or bus.
- 4) Engine hours (or mileage) are taken from hour meters or odometers installed on the equipment.
- 5) After engine stabilization, the exhaust gas sampling probe is inserted into the exhaust stream. The Autocal button is depressed and after the LED readouts clear, test personnel take multiple readings of carbon dioxide, carbon monoxide, unburned hydrocarbons, and oxygen, along with engine speed, exhaust temperature and pressure. Smoke readings are taken on the diesel engines after exhaust gas testing.
- 6) Periodically, ambient air temperature, atmospheric pressure, and relative humidity are recorded. Temperature readings are taken at the test site. Other ambient readings are acquired from local weather information services.
- 7) All data are recorded until technicians are confident the information is consistent and reproducible.
- 8) After completing the baseline, the test fleet fuel was treated with FPC-1. All equipment operated as normal for approximately 400 to 500 hours, at which time the above procedure was reproduced without alteration, except FPC-1 fuel treatment in the test fleet.

V. Discussion

The data collected during the tests are summarized on the attached computer printouts (Appendix 1). From these data the volume fraction (VF) of each gas is determined and the average molecular weight (Mwt) of the exhaust gases computed. Next, the engine performance factor (pf) based upon the carbon mass in the exhaust is computed. The pf is finally corrected for intake air temperature and pressure (barometric), and total exhaust mass yielding a corrected

engine performance factor (PF). The PFs for the diesel engines are tabulated on Table 1 of Appendix 3. The carbon monoxide percentages are tabulated on Table 2 of Appendix 3. The smoke spot (smoke density) numbers for the diesel engines are found on Table 3 of Appendix 3.

Fuel consumption was reduced by 11.6% in the BEC/allwaste study. This is a slightly larger change than observed in prior tests on similar equipment. The results are consistent from engine to engine, therefore, the confidence level in the results is high. However, it is most likely that the reduction in fuel consumption will be similar to that observed by other fleets under actual operating conditions (8% to 9%).

VI. Conclusions

- (1) The addition of FPC-1 to the diesel fleet created an 11.63% reduction in fuel consumption.
- (2) Unburned hydrocarbon emissions were reduced 22.2% on a fleet average basis.
- (3) Smoke density was reduced 23.9% after FPC-1 fuel treatment.

Company Name:	BEC Allwaste	Location:	Birmingham		Date:	7/10/96
Test Portion:	Baseline	Stack Diam.	5	Inches		
Engine Type:	Cummins 400	Mile/Hrs	435249			
Equipment Type:		ID #:	1247		Baro	30.08
Fuel Sp. Gravity(SG	.850	Temp:	68			
					Time:	8:35

RPM	Exh Temp	Pv Inch	CO	He	CO2	O2	
2200	381	1.05	0.04	36	1.86	18.3	
2200	382	1.05	0.04	35	1.86	19	
2200	381	1.05	0.04	36	1.86	19	
2200	382	1.05	0.04	35	1.83	18.9	
2200	382	1.05	0.04	35	1.83	18.9	
2200	383	1.05	0.04	36	1.86	19	
2200	383	1.05	0.04	37	1.84	19	
2200.000	382.000	1.050	.040	35.714	1.849	18.871	Mean
, 0	.816	.000	.000	.756	.015	.256	Std Dev

VFHC	VFCO	VFCO2	VFO2	Mtw1	pf1	PF1
3.57E-05	0.0004	.018	.189	29.053	339,177	405,879

Company Name:	BEC Allwaste	Location:	Birmingham		Test Date:	9/12/96
Test Portion:	Treated	Stack Diam:	5	Inches		
Engine Type:	Cummins 400	Mile/Hrs:	444766			
Equipment Type	Kenworth	ID #:	1247		Baro:	29.92
Fuel Sp. Gravity: SG Corr Factor:	.850 1.000	Temp:	64		Time:	7:40

RPM	Exh Temp	Pv Inch	CO	HC	CO2	O2	
2200	374.4	1.05	0.04	28	1.63	19.2	
2200	374	1.05	0.03	30	1.62	19.2	
2200	372.8	1.05	0.04	30	1.62	19.3	
2200	373.2	1.05	0.03	31	1.63	19.3	
2200	372	1.1	0.03	32	1.63	19.3	
2200	371.4	1.1	0.03	32	1.61	19.4	
5.7							
2200.000	372.967	1.067	.033	30.500	1.623	19.283	Mean
0	1.148	.026	.005	1.517	.008	.075	Std Dev

VFHC	VFCO	VFCO2	VFO2	Mtw2	pf2	PF2
3.05E-05	0.000333333	.016	.193	29.033	386,513	455,214

Performance factor adjusted for fuel density:

455,214

**% Change PF= 12.16 %

Company Name:	BEC Allwaste	Location:	Birmingham		Date:	7/10/96
Test Portion:	Baseline	Stack Diam.	5	Inches		
Engine Type:	Cat 3406	Mile/Hrs	112701			
Equipment Type:	Lo Boy	ID #:	4368		Baro	30.08
Fuel Sp. Gravity(SG	.845	Temp:	70			
					Time:	9:00

RPM	Exh Temp	Pv Inch	CO	FI(6)	CO2	02	
1800	309	0.5	0.01	8	1.68	19.1	
1800	310.4	0.5	0.01	7	1.65	19.1	
1800	311.4	0.5	0.01	9	1.65	19.1	
1800	311.2	0.5	0.01	10	1.64	19	
1800	312	0.55	0.01	10	1.64	19.3	
1800	312	0.55	0.01	10	1.67	19.3	
1800	313	0.55	0.01	10	1.65	19.3	
1800	313.4	0.55	0.01	10	1.66	19.2	
1800.000	311.550	.525	.010	9.250	1.655	19.175	Mean
0	1.409	.027	.000	1.165	.014	.116	Std Dev

VFHC	VFCO	VFCO2	VFO2	Mtw1	pf1	PF1
9.25E-06	0.0001	.017	.192	29.032	387,729	628,117

Company Name:	BEC Allwaste	Location:	Birmingham		Test Date:	9/12/96
Test Portion:	Treated	Stack Diam:	5	Inches		
Engine Type:	Cat 3406	Mile/Hrs:	121613			
Equipment Type	Lo Boy	ID #:	4368		Baro:	29.92
Fuel Sp. Gravity: SG Corr Factor:	.844 1.001	Temp:	64		Time:	8:00

RPM	Exh Temp	Py Inch	CO	HC	CO2	02	
1800	308.4	0.5	0.01	6	1.52	19.2	
1800	309.4	0.5	0.01	6	1.5	19	
1800	310.5	0.5	0.01	6	1.51	19.5	
1800	310.8	0.5	0.01	6	1.51	19.6	
1800	311.4	0.55	0.01	9	1.5	19.5	
1800	312.2	0.55	0.01	7	1.49	19.5	
1800	312.6	0.55	0.01	6	1.48	19.6	
1800.000	310.757	.521	.010	6.571	1.501	19.414	Mean
0	1.492	.027	.000	1.134	.013	.227	Std Dev

VFHC	VFCO	VFCO2	VFO2	Mtw2	pf2	PF2
6.57E-06	0.0001	.015	.194	29.017	427,231	692,271

Performance factor adjusted for fuel density:

693,090

**% Change PF=

10.34 %

Company Name: BEC Allwaste Location: Birmingham Date: 7/10/96

Test Portion: Baseline Stack Diam. 4 Inches

Engine Type: Cat 3114 Mile/Hrs 5384

Equipment Type: Front End Loader ID #: Baro 30.08

Fuel Sp. Gravity(SG .842 Temp: 70

Time: 9:30

RPM	Exh Temp	Pv Inch	C (0)	HC	CO2	O2	
2538	439	0.7	0.01	6	2.45	18.5	
2538	445.8	0.7	0.01	7	2.46	18.4	
2538	455	0.7	0.01	8	2.44	18.5	
2538	455	0.7	0.01	6	2.45	18.5	
2538	457.8	0.7	0.01	8	2.42	18.5	
2538	458	0.7	0.01	8	2.41	18.5	
2538	457	0.7	0.01	6	2.4	18.5	
2538.000	452.514	.700	.010	7.000	2.433	18.486	Mean
0	7.283	.000	.000	1.000	.023	.038	Std Dev

 VFHC
 VFCO
 VFCO2
 VFO2
 Mtw1
 pf1
 PF1

 7.00E-06
 0.0001
 .024
 .185
 29.129
 265,605
 633,193

Company Name: BEC Allwaste Location: Birmingham Test Date: 9/12/96

Test Portion: Treated Stack Diam: 4 Inches

Engine Type: Cat 3114 Mile/Hrs:

Equipment Type Front End Loader ID #: Baro: 29.92

 Fuel Sp. Gravity:
 .847
 Temp:
 62

 SG Corr Factor:
 .994
 Time:
 9:00

RPM Exh Temp Pv Inch CO HC CO2 **O2** Full 0.7 0.01 416.4 2.18 18.7 416.4 0.7 0.01 4 Full 2.18 18.7 Full 414.4 0.75 0.01 4 2.17 18.9 Full 414.4 0.75 0.01 2.15 18.9 413.2 0.75 Full 0.01 2.16 18.9 Full 413.2 0.75 0.01 2.15 18.8 Full 412.8 0.75 0.01 2.15 18.9 Full 412.8 0.75 0.01 2.15 18.8 #DIV/0! 414.200 .738 .010 4.000 2.161 18.825 Mean #DIV/0! 1.497 Std Dev .023 .000 .000 .014 .089

VFHC VFCO VFCO2 VFO2 Mtw2 pf2 PF2 4.00E-06 0.0001 .022 .188 29.099 298,717 677,261

Performance factor adjusted for fuel density: 673,239 **% Change PF = 6.32 %

Company Name:	BEC Allwaste	Location	Birmingham		Date:	7/10/96
Test Portion:	Baseline	Stack Diam.	4	Inches		
Engine Type:	Cummins 5.9	Mile/Hrs	131507			
Equipment Type:	Ford Lube Truck	ID #;	1442		Baro	30.07
Fuel Sp. Gravity(SG	.845	Temp:	70			
					Time:	9:50

RPM	Exh Temp	Pv Inch	CO	HC	CO2	02	
2500	381.4	1.25	0.03	9	1.79	18.9	
2500	377	1.25	0.03	10	1.8	18.9	
2500	378	1.25	0.03	10	1.78	18.8	
2500	379	1.25	0.03	9	1.78	19	
2500.000	378.850	1.250	.030	9.500	1.788	18.900	Mean
0	1.886	.000	.000	.577	.010	.082	Std De

VFHC	VFCO	VFCO2	VFO2	Mtw1	pf1	PF1
9.50E-06	0.0003	.018	.189	29.043	355,395	607,794

Company Name:	BEC Allwaste	Location:	Birmingham		Test Date:	9/12/96
Test Portion:	Treated	Stack Diam:	4	Inches		
Engine Type:	Cummins 5.9	Mile/Hrs:	139784			
Equipment Type	Ford Lube Truck	ID #:	1442		Baro:	29.92
Fuel Sp. Gravity: SG Corr Factor:	.845 1.000	Temp:	62		Time:	9:30

RPM	Exh Temp	Pv Indi	€0	11(6	CO2	0)2	
2500	374.4	1.25	0.03	6	1.53	19	
2500	385.4	1.25	0.03	6	1.53	18.9	
2500	371	1.25	0.03	6	1.53	19.3	
2500	375.4	1.35	0.03	7	1.52	19.2	
2500	379.6	1.35	0.03	8	1.52	19.2	
			п				
2500.000	377.160	1.290	.030	6.600	1.526	19.120	Mean
0	5.534	.055	.000	.894	.005	.164	Std Dev

VFHC	VFCO	VFCO2	VFO2	Mtw2	pf2	PF2
6.60E-06	0.0003	.015	.191	29.009	414,909	696,040

Performance factor adjusted for fuel density:

696,040

**% Change PF= 14.52

Company Name:	BEC Allwaste	Location	Birmingham		Date:	7/10/96
Test Portion:	Baseline	Stack Diam.	5	Inches		
Engine Type:	Cat 3406-B	Mile/Hrs	393677			
Equipment Type:	Lo Boy	ID #:	9354		Baro	30.07
Fuel Sp. Gravity(SG	.844	Temp:	72			
					Time:	10:00

RPM	Exh Temp	Pv Inch	CO	HC	CO2	O2	
1855	309	0.35	0.02	8	1.31	19.4	
1855	312.8	0.35	0.02	8	1.29	19.4	
1855	319	0.35	0.02	7	1.29	19.4	
1855	319	0.35	0.02	7	1.31	19.4	
1855	320	0.35	0.02	. 8	1.33	19.4	
1855	320	0.35	0.02	8	1.32	19.4	
1855.000	316.633	.350	.020	7.667	1.308	19.400	Mean
0	4.622	.000	.000	.516	.016	.000	Std Dev

VFHC	VFCO	VFCO2	VFO2	Mtw1	pf1	PF1
7.67E-06	0.0002	.013	.194	28.986	485,152	965,584

Company Name:	BEC Allwaste	Location:	Birmingham		Test Date:	9/12/96
Test Portion:	Treated	Stack Diam:	5	Inches		
Engine Type:	Cat 3406-B	Mile/Hrs:	402736			
Equipment Type	Lo Boy	ID #:	9354		Baro:	29.92
Fuel Sp. Gravity: SG Corr Factor:	.850 .993	Temp:	62		Time:	10:20
SG COTT PACIOT:	.993				1 imet	10:20

RPM	Exh Temp	Pylinch	CO	ile	CO2	O2	
1865	304.4	0.35	0.02	7	1.1	19.7	
1865	307.4	0.35	0.02	7	1.09	19.6	
1865	310.8	0.35	0.02	6	1.09	19.7	
1865	311.8	0.35	0.02	6	1.09	19.7	
1850	316.8	0.4	0.02	6	1.07	19.8	
1850	314	0.4	0.02	6	1.07	19.8	
1850	313.4	0.4	0.02	5	1.08	19.8	
1850	313.2	0.4	0.02	5	1.07	19.8	
1857.500	311.475	.375	.020	6.000	1.083	19.738	Mean
8.017837257	3.939	.027	.000	.756	.012	.074	Std Dev

VFHC	VFCO	VFCO2	VFO2	Mtw2	pf2	PF2
6.00E-06	0.0002	.011	.197	28.963	584,194	1,116,746

Performance factor adjusted for fuel density:

1,108,807

**% Change PF = 14.83 %

APPENDIX 3

Table 1. Changes in Fuel Flow Rate (PFs)

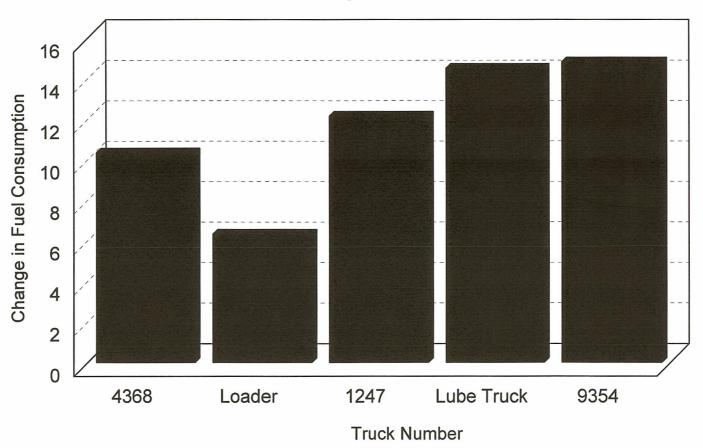
Unit #	Base PF	FPC PF	% Change
4368 Loader 1247 Lube Truck 9354	628,117 633,193 405,879 607,794 965,584	693,090 673,239 455,214 696,040 1,108,807	10.34 6.32 12.16 14.52 14.83
		Fleet Average:	11.63

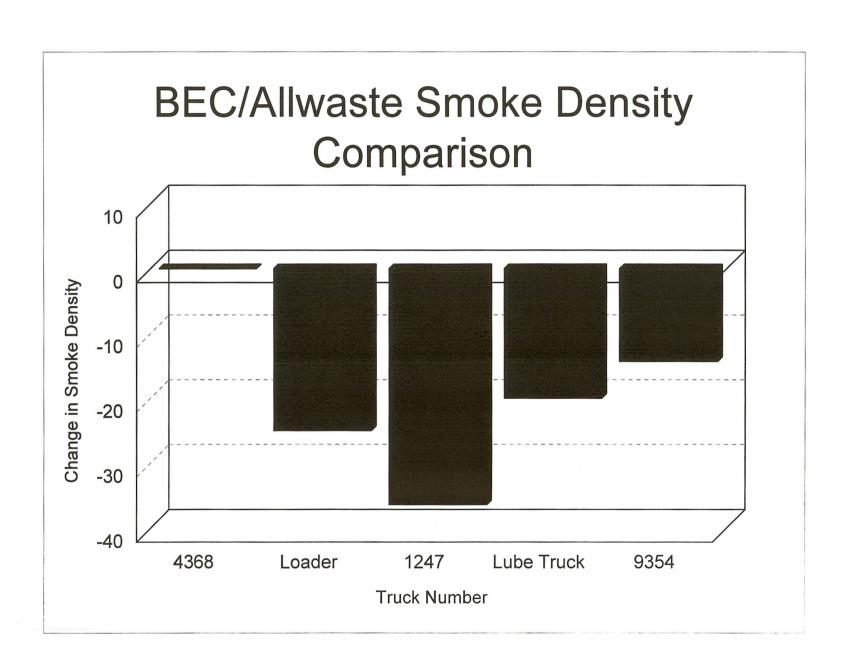
Note: An increase in PF equals a reduction in fuel consumption since the PF is a measure of the length of time required to consumed the same amount of fuel. The more efficient the engine, the longer it takes to consume the same amount of fuel, so the PF is higher.

Table 2. Changes in Smoke Density (Smoke Spot Numbers)

<u>Unit #</u>	Base No.	FPC No.	% Change
4368 Loader 1247 Lube Truck 9354	na 4.0 5.5 5.0 7.0	4.0 3.0 3.5 4.0 6.0	na -25.0 -36.4 -20.0 -14.3
		Fleet Average	-23 0







APPENDIX 4

Figure 1 CARBON MASS BALANCE FORMULAE

ASSUMPTIONS: $C_{12}H_{26}$ and SG = 0.82

Time is constant Load is constant

DATA: Mwt = Molecular Weight

pf1 = Calculated Performance Factor (Baseline) pf2 = Calculated Performance Factor (Treated)

PF1 = Performance Factor (adjusted for Baseline exhaust mass)
PF2 = Performance Factor (adjusted for Treated exhaust mass)

CFM = Volumetric Flow Rate of the Exhaust

SG = Specific Gravity of the Fuel

VF = Volume Fraction

d = Exhaust stack diameter in inches Pv = Velocity pressure in inches of H₂0

 $P_{\rm B}$ = Barometric pressure in inches of mercury

Te = Exhaust temperature ${}^{o}F$

VFHC = "reading" \div 1,000,000

VFCO = "reading" \div 100 VFCO₂ = "reading" \div 100 VFO₂ = "reading" \div 100

EQUATIONS:

Mwt =

(VFHC)(86)+(VFCO)(28)+(VFCO₂)(44)+(VFO₂)(32)+[(1-VFHC-VFCO-VFCO₂-VFO₂)(28)]

pf1 or pf2 = $\frac{3099.6 \text{ x Mwt}}{86(\text{VFHC}) + 13.89(\text{VFCO}_2)}$

CFM = $\frac{(d/2)^2 \pi}{144} \left(1096.2 \sqrt{\frac{Pv}{1.325(PB|ET+460)}} \right)$

 $PF1 \text{ or } PF2 = \underbrace{pf \text{ x (Te+460)}}_{CFM}$

FUEL ECONOMY:
PERCENT INCREASE (OR DECREASE)

<u>PF2 - PF1</u> x 100

Figure 2.

SAMPLE CALCULATION FOR THE CARBON MASS BALANCE

BASELINE:

Equation 1 (Volume Fractions)

VFHC = 13.20/1,000,000 = 0.0000132 VFCO = 0.017/100 = 0.00017 VFCO₂ = 1.937/100 = 0.01937 VFO₂ = 17.10/100 = 0.171

Equation 2 (Molecular Weight)

Mwt1 = (0.0000132)(86) + (0.00017)(28) + (0.01937)(44) + (0.171)(32)+ [(1-0.0000132-0.00017-0.01937-0.171)(28)]

Mwt1 = 28.995

Equation 3 (Calculated Performance Factor)

pf1 =
$$\frac{3099.6 \times 28.995}{86(0.0000132) + 13.89(0.00017) + 13.89(0.01937)}$$

pf1 = 329,809

Equation 4 (CFM Calculations)

CFM =
$$\frac{(d/2)^2 \pi}{144} \left(1096.2 \sqrt{\frac{P_V}{1.325(PB/ET + 460)}} \right)$$

d =Exhaust stack diameter in inches

Pv = Velocity pressure in inches of H_20

P_B = Barometric pressure in inches of mercury

Te = Exhaust temperature ${}^{0}F$

CFM =
$$\frac{(10/2)^2 \pi}{144} \left(1096.2 \sqrt{\frac{.80}{1.325(30.00/313.100 + 460)}} \right)$$

CFM = 2358.37

Equation 5 (Corrected Performance Factor)

PF1 =
$$329.809(313.1 \text{ deg F} + 460)$$

2358.37 CFM

PF1 = 108,115

TREATED:

Equation 1 (Volume Fractions)

$$VFCO_2 = 1.826/100$$

= 0.01826

$$VFO_2 = 17.17/100$$

= 0.1717

Equation 2 (Molecular Weight)

Mwt2 =
$$(0.0000146)(86) + (0.00013)(28) + (0.01826)(44) + (0.1717)(32)$$

+ $[(1-0.0000146-0.00013-0.01826-0.1717)(28)]$

$$Mwt2 = 28.980$$

Equation 3 (Calculated Performance Factor)

pf2 =
$$\frac{3099.6 \times 28.980}{86(0.0000146) + 13.89(0.00013) + 13.89(0.01826)}$$

pf2 = $349,927$

Equation 4 (CFM Calculations)

CFM =
$$\frac{(d/2)^2 \pi}{144} \left(1096.2 \sqrt{\frac{P_V}{1.325(PB[ET+460])}} \right)$$

d = Exhaust stack diameter in inches

Pv = Velocity pressure in inches of H₂0

P_B =Barometric pressure in inches of mercury

Te =Exhaust temperature ^oF

CFM =
$$\frac{(10/2)^2 \pi}{144} \left(1096.2 \sqrt{\frac{.775}{1.325(29.86/309.02 + 460)}} \right)$$

CFM = 2320.51

Equation 5 (Corrected Performance Factor)

PF2 =
$$349.927(309.02 \text{ deg } F + 460)$$

2320.51 CFM

= 115,966

Fuel Specific Gravity Correction Factor

Baseline Fuel Specific Gravity - Treated Fuel Specific Gravity/Baseline Fuel Specific Gravity +1

$$.840 - .837 / .840 + 1 = 1.0036$$

$$PF2 = 115,966 \times 1.0036$$

$$PF2 = 116,384$$

Equation 6 (Percent Change in Engine Performance Factor:)

% Change PF =
$$\frac{PF2 - PF1}{PF1} \times 100$$

Note: A positive change in PF equates to a reduction in fuel consumption.

APPENDIX 2

7	ERRY	Car	bon Mass	Balance	Field I	ata For	m		
Cor Tes	mpany: 1	Baseline:	eske Locatio	on: B- H ated:	_ Exha	Test I ust Stack I	Date: 7 Diameter	/10/96 4 Inches	
Enį Tyj	une Make be of Equi	/Model: <u>Cu</u> pment: <u>Fe</u>	m 5,9	Hue	Ailes/Hou	irs: <u>/3/</u> 50	?≥ I.D.#	1442	
Bar	ometric P	ressure:	1845	Inche	s of Mer	cury	9.		Water temp Conter
	RPM	The State of the S	P.Inches A for H.O.	% <u>CO</u>	HC/	% CO ₂	%:02°	ASmoke Simpler	A C
	2500	38/4	1,05	103	9		/	5	fan ok
		377.	1,25	103	9	16.7	18,9		
			1,25	103	103,	1814	1819		:- <u>*</u>
-		3-/8	1.25	103	10	1,78	1816		
		7		,03	10	1,73	1911	·	· .
		579	:	103	4	117.8	19.		
					-1			••	
							ie.		
							÷		
			•		Е	and Time_	10:0	<u></u>	l este je

FT-12

ine Ma e of Eq	ke/Model: <u>Cu</u> juipment: <u>F</u> r	ontend h	4 A	Ailes/Ho	urs: <u>5384</u>	I.D.#	<i>!</i> :	le.
metric	Tic Gravity: Pressure: Temperature: _		Inche	s of Mei	@:_ cury Start Time:_			Do
RPM		Princies y for H.O	% CO	HC ppm+	%:CO.	% O.F	Smoke Number	
	439	707	101	6	2.45	18.5	4	
	44518		,01	7	2,46	1814	/	XI.
	435		101	8	2,44	1815		
	455	107	101	6	2,45	18,5		P1
	457,8		101	8	3.42	1815		0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	458	, 7	101	8	2,41	18,5		
3	457		,01	6	2,40	1815		
2		1						
T.				-				
					End Time			

Signature of Technicians:

Company: BEC Allurate Location: Brest Portion: Baseline: X Treated:	Exhaust Stack Diameter:Inches
Engine Make/Model: <u>Cut 3406-B</u> Type of Equipment: 10 bou	_Miles/Hours:393677 I.D.#: \$9.9354
Fuel Specific Gravity:,&44Inc	@: (°F) ches of Mercury F) Start Time:

RPM.	Exhaust Temp F	P Inches of H 0	% GO	HC ppm	% CO2	% O.	Smoke Number
1835	308	,35	,,,,3	8	1,37	19,4	
	309	7,	,02	8	<i>1</i> ,3/	19,4	·
	3//		102	8	1.35	19,4	
	3128	.35	102	8	1,29	19,4	1 (1)
	3,9		,01	7	1,29	19.4	
	3,9		102	7	1,3j	19.4	
	370	35	102	8	/, <i>3</i> 3	19,4	
	320		,03	8	1,34	151	. ••
	;		* 8	·			
		·	·		·		

End Time_

Specific	Gravity:	X Tre 6 Cat, 1000446 3406	-1-7-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-		@:	J_ 1.D.#		EAN DOWN NG
ometric Pr ke Air Te				es of Mero S	cury tart Time:_	8:0	<u>U</u>	
RPM	Exhausta Temp F	P.Inches V.	% CO	HC ppm	The second second	% O. T.	Smoke Number	
2000	342.	.7	,0/	6	1.73	19,	4	
	340	7,	101	8	1,73	189		
	339		.01	5	1.72	19.2		Acon fux o
	339		.01	5	1.72	19.0	~	
	338	e 7	.01	5	1.75	19.3		
	338	. 5	.01	5	1.73	19.3		
	338	07	,01	5	1.73	19.2		
			.,				••	

Carbon Mass Balance Field Data Form Company: B Alwar Location: B-ham Test Date: 7/10/96 Test Portion: Baseline: Y Treated: Exhaust Stack Diameter: Inches Engine Make/Model: 14 376 _____ Miles/Hours: 1270 1 I.D.#: 4368 Type of Equipment: ____ Fuel Specific Gravity: 1845 Inches of Mercury Barometric Pressure: Start Time: 9100) Intake Air Temperature: (°F) P Inches of H₂O Temp F. Vumber 1800 309 101 3101 10 10 311, 2 3/2.0 101 ,01 101 10 101

End Time

Cor Tes	Company: 3± 4 Al Location: B-han Test Date: 7/0/96 Test Portion: Baseline: X Treated: Exhaust Stack Diameter: 5 Inches									
Eng Tyj	ine Make/ oc of Equip	Model: <u>Um</u> oment: <u>A</u>	EN WOATH	YN	1iles/Hou	rs <u>4359</u> 9	19 I.D.#	1247		
Fuel Specific Gravity: (°F) Barometric Pressure: Inches of Mercury Intake Air Temperature: (°F) Start Time: 3'.35										
	RPM		P Inches 14 for H ₂ O	% CO	HC ppm	% CO.	% O.1	Smoke Number	160 160	
	<u> </u>	381,4	1.05	, 04	35	1,91	18	5.5	C. 1 1 cm	
		38 /	1.05	-04	36	1.86	18,3			
		382	1.05	.04	35	1.86	19,0		Or 1	
		381	1.05	.04	36	1.80	19.0			
		382	1.05	.c.4	35	1.83	18.9			
		382	1,05	.04	35	1.83	18.9	·		
		383	1.05	,04	36		19.0	,	9 ° 1 9 9 9	
		383	1.05	,04	37	1.84	19.0	••	÷	
			(,,,			7) ,		·		

End Time 8:50

Company: Bec/ALLMASTE L	ocation: Blammyhan	Test Date:	7-12-96
Test Portion: Baseline:	Treated:E	chaust Stack Diamete	r:Inches
Engine Make/Model: CAT 3	406 - B Miles/1	Hours: 402736 I.D	# 9354
Type of Equipment: LoBoy Fo) k()		
Fuel Specific Gravity:	50	@:	(°F)
Barometric Pressure:	Inches of N	Mercury	
Intake Air Temperature:	(°F)	Start Time:	

RPM (Exhausta	P Inches	%CO	HC	% CO ₂ ;	%.O ₂	Smoke
	Temp*F.	of H ₂ O		ppm :			Number
1865	304.4	. 35	. 62	7	110	19.7	6.6
1	307.4	.35	.02	7	1.09	19.4	
1865	310.8	. 35	,02	6	1.09	19.7	
	311:8	. 35	.07	40	1.09	19.7	
1850	316.8	.40	.02	6	1.07	19.8	
1	314.0	.40	.62	6	1.07	15.8	•
1850	313.4		-67	5	1.68	19.8	¥
4	3/3,2		.02	5	1.67	19.8	, ••
		•	•	I	End Time_		

FAN-OFF AC-OFF

Company: Q Cest Portion:	EC/ALLWAIT Baseline:	Locatio Tres	n: B.4m 7 ated:_ X	Exha	Test I	Date: <u>9</u> Diameter:	-12-96 5 Inches	
Engine Make.	/Model:K	mm,n65						
Barometric P	Gravity: ressure: emperature: _		 Inche (°F)	es of Mero S	211	714	_(°F) O_Am	
RPM.	Exhausta Temp °F	P Inches 4	% Ĉ Ö	HC ppm	% CO ₂	% O.	Smoke Number	H/C of I
2200	374,4	1.05	104	28	1.63	19,2	3,5	FAN-ON
		1.05						160°F
	3728		,04	30	1,62	19,3		011 Tom
	373.2	2 W W	103	9	A	19.3		
	372.	1,10						
	3//,4	1.10	103	32	1.6]	17,4		
							••	
					·			aca.
		,		I I	End Time	X:15	0.4	

WADE	
Miss	

Con Test	pany: 2 Portion:	Baseline:	Locatio Tres	n: Biem ated:	exhau	Test I ust Stack I	Date: 9 Diameter:	-12-94 Inches	
Eng Typ	ine Make/ c of Equip	Model: Coroment:]	mmys 5	1.9 182	Ailes/Hou	ırs: <u>/347</u> (₹ I.D.#	1042	
Bar	ometric Pr	Gravity: essure: mperature: _		Inche	s of Mer	cury		(°F)	TEMP CONTER
	RPM I	Exhaust A Temp F.	P.Inches A Vof H,O	%(CO)	HC ppm r	% CO ₂	% O.T.	Smoke s Number	AC-01 FAN-0
	2500	374.4	1.25	102	4	1.55	19.0	4	
		385.4		102	4	1.53	18.9		
		371.0		, 03	6	1.53	19.3		
-		375.4	1.35	,63	7	1.52	19.2		
		375.4	1.35	.03	8	1.55	19.2		
		379.4	. 1/35	.03	8	1.52	14.2	·	
		379.0	1.35	, = 3	ク	1.56	19.2		
								. ••	
			,						*
1			•	•	F	End Time_	16:20	DA	

Signature of Technicians:

TERRS CAUDLE

		Car	bon Mass	Balance	Field D	ata For	m		
Cor Tes	npany: 3 i Portion	Baseline:	Locatio	n: Biemii ated:	yham Exhau	Test I ust Stack I	Date: <u>9</u> -	-12-96 Inches	
Enj	ıne Mal	cc/Model:	AT 3114						
Bai	ometric	Te Gravity: Pressure: Temperature: _		Inche	es of Mero S	cury			Water
	RPM	Exhaust Temp 2F3	P.Inches A. Tor H.O.	% CO	HC ppm		% O ₂	Smoke Number	186°F
	FULL	416.4	.7	, 6]	4	2.18	18.7	3	
		416.4	+	.01	4	2:18	18.7		
		414.4	.75	.01	4	2.17	18.9		
		4144	1	.01	4	2.15	18.4		
		413.2	.75	-01	4	2.16	18.9		
		413.2	1 1	.01	4	2.15	1828		en . .ange
		412.8	.75	.01	4	2.15	189		7
	1	412.8	1	-61	4	2.15	18.8	. ••	14 Jan 14
			,						and the second
					I	End Time_		-	

	Car	bon Mass	Balance	Field L	Pata For	m		
ompany: <u>B</u> e est Portion:	Baseline:	Locatio Tre	n: Biomin ated:	gham Exhan	Test I	Date: 9 : Diameter:	12-9 L Inches	
ngine Make. ype of Equi	/Model: <u>CA7</u> pment:	340	6N	Ailes/Hou	ırs: <u>!2[6]</u>	<u>3</u> I.D.#	4368	
arometric P	ressure:	. 844	Inche	es of Mero S	cury			
RPM	Exhaust Temp°F	P.Inches . of H.O.	% CO	HC ppm	% CO ₂	% O.	Smoke Number	
1800	308.4	0.56	,01	4	1.52	19.2	4	FAN- AC-
1800	309.4	0.50	.01	6	1.50	19.0		
1800	310.5	0.50	.01	4	1.51	19.5		
1800	310.8	0.50	-01	4	1.51	19.6		
1800	311.4	0.55	.01	9	1.50	19.5		
1800	312.2	. 0.55	101	7	1.49	19.5		
1860	312.6	0.55	.61	4	1.48	19.6		
			1			2	••	
		,						
					·		1	
				I	End Time_			B. San

JAMES	
SHIPS	

APPENDIX 5



HIGH TECHNOLOGY SOLUTIONS TO CURRENT ENVIRONMENTAL CHALLENGES

Time	Pressure	Temp
12am	29.97	72
lam	29.98	72
2am	29.99	72
3am	29 . 9 9	71
4am	29.99	71
5am	30.01	69
6am	30.03	68
7am	30.05	65
Sam	30.08	68
9am		No Report
10am		No Report
1 lam		No Report
12pm		No Report
1pm		No Report
2pm		No Report
3pm		No Report
4pm	30.06	85

Michael J. Ruvcce
Information Management & Customer Service
WeatherBank, Incorporated

WBI1	More info on how to call up WeatherBank files
WIND	How to get specific upper level wind forecasts
WWC	How to obtain the NWS Weekly Crop outlook
ZONES	How to obtain the new NWS state zone forecasts Interactively
800NET	More information on the 800 network and prices
7DTF	How to call up 7-day temperature forecasts

EXAMPLE:

HELP HOURLY Will call up help on the HOURLY command.

NOTES:

- To download information about the WeatherBrief Software and how to obtain the service, type HELP INFO.
- To control data flow, hit a <CONTROL> S to pause, and <CONTROL> Q to go.
- To kill current command in a command file, hit a <CONTROL> X.
- To abort transmission of any product, hit a single CONTROL C.
- To recall last command, hit a <CONTROL> R.

STATION FILE: AL	09-3	12-08	GM?	[
DY-HR TOWN					WIND GST	PRSSR	VSB	LY-WX	CLOUD COVER
=======================================					=======				==========
12-08A*Muscle Shoal									
12-09A*Muscle Shoal									
12-10A*Muscle Shoal									
12-11A Muscle Shoal	62	60	93	62	W 4	29.97	3	BR	SKC
12-12P Muscle Shoal		60	100		W 4	29.98	3	BR	SKC
12-01P Muscle Shoal		64	93		NW 4	29.98	3	BR	SKC
12-02P Muscle Shoal		64	79		NW 5	29.98	5	HZ	SKC
12 021 masere shoar	,	0 1	, ,	0,5	2111 3	23.30	, ,		Site
DY-HR TOWN	TMP	DEW	HUM	FLK	WIND GST	PRSSR	VSB	LY-WX	CLOUD COVER
=======================================	===	===	===	===	=======	=====			==========
12-08A Huntsville	62	62	100	62		29.93	5	BR	CLR
12-09A Huntsville	60	60	100		NW 5	29.95	4	BR	CLR
12-10A Huntsville	60	60	100	60	NW 4	29.96	7		CLR
12-11A Huntsville	60	60	100	60	N 0	29.96	7		CLR
12-12P Huntsville	60	60	100	60	N = 0	29.98	7		CLR
12-01P Huntsville	64	62	93	64	N 0	29.98	7		CLR
12-02P Huntsville	69	62	79	69	N 0	29.98	6	HZ	CLR
DY-HR TOWN	TMP	DEW	MUH	FLK	WIND GST	PRSSR	VSB.	LY-WX	CLOUD COVER
=======================================	===	===	===	===	=======	=====	===	=====	=======================================
===== ================================	=== 66	=== 64	93	=== 66	N 0	===== 29.91	=== 5	==== BR	SKC
12-08A Tuscaloosa 12-09A Tuscaloosa	=== 66 64	=== 64 64	=== 93 100	=== 66 64	N 0 N 0	===== 29.91 29.91	=== 5 4	BR BR	SKC SKC
12-08A Tuscaloosa 12-09A Tuscaloosa 12-10A Tuscaloosa	=== 66 64 64	=== 64 64 64	93 100 100	=== 66 64 64	N 0 N 0 N 0	==== 29.91 29.91 29.90	=== 5 4 5	BR BR VCFG	SKC SKC SKC
12-08A Tuscaloosa 12-09A Tuscaloosa 12-10A Tuscaloosa 12-11A Tuscaloosa	=== 66 64	=== 64 64 64 62	93 100 100 93	=== 66 64 64 64	N 0 N 0 N 0 N 0 N 0	==== 29.91 29.91 29.90 29.90	5 4 5 5	BR BR VCFG BR	SKC SKC SKC SKC SKC
12-08A Tuscaloosa 12-09A Tuscaloosa 12-10A Tuscaloosa 12-11A Tuscaloosa 12-12P Tuscaloosa	=== 66 64 64	=== 64 64 64	93 100 100 93 93	=== 66 64 64 64 62	N 0 N 0 N 0 N 0 N 0 N 0	==== 29.91 29.91 29.90	5 4 5 5 5	BR BR BR VCFG BR BR	SKC SKC SKC SKC SKC SKC
12-08A Tuscaloosa 12-09A Tuscaloosa 12-10A Tuscaloosa 12-11A Tuscaloosa 12-12P Tuscaloosa 12-01P Tuscaloosa	=== 66 64 64 64 64	=== 64 64 64 62 62 64	93 100 100 93 93 87	=== 66 64 64 64 62 66	N 0 N 0 N 0 N 0 N 0 N 5 N 5	==== 29.91 29.91 29.90 29.90	5 4 5 5 5 6	BR BR VCFG BR	SKC SKC SKC SKC SKC SKC SKC
12-08A Tuscaloosa 12-09A Tuscaloosa 12-10A Tuscaloosa 12-11A Tuscaloosa 12-12P Tuscaloosa	=== 66 64 64 64	=== 64 64 64 62 62	93 100 100 93 93	=== 66 64 64 64 62 66	N 0 N 0 N 0 N 0 N 0 N 0	29.91 29.91 29.90 29.90 29.95	5 4 5 5 5	BR BR BR VCFG BR BR	SKC SKC SKC SKC SKC SKC
12-08A Tuscaloosa 12-09A Tuscaloosa 12-10A Tuscaloosa 12-11A Tuscaloosa 12-12P Tuscaloosa 12-01P Tuscaloosa 12-02P Tuscaloosa	=== 66 64 64 64 64 68 73	=== 64 64 64 62 62 64 66	93 100 100 93 93 87 79	=== 66 64 64 64 62 66 76	N 0 N 0 N 0 N 0 N 0 N 5 N 5 NE 5	29.91 29.91 29.90 29.90 29.95 29.96	=== 5 4 5 5 5 6 7	BR BR VCFG BR BR BR	SKC SKC SKC SKC SKC SKC SKC
12-08A Tuscaloosa 12-09A Tuscaloosa 12-10A Tuscaloosa 12-11A Tuscaloosa 12-11P Tuscaloosa 12-01P Tuscaloosa 12-02P Tuscaloosa DY-HR TOWN	=== 66 64 64 64 64 68 73	=== 64 64 64 62 62 64 66	93 100 100 93 93 87 79	=== 66 64 64 64 62 66 76 FLK	N 0 N 0 N 0 N 0 N 0 N 5 N 5 NE 5 WIND GST	29.91 29.91 29.90 29.90 29.95 29.96 PRSSR	=== 5 4 5 5 5 6 7	BR BR VCFG BR BR BR	SKC
12-08A Tuscaloosa 12-09A Tuscaloosa 12-10A Tuscaloosa 12-11A Tuscaloosa 12-11P Tuscaloosa 12-01P Tuscaloosa 12-02P Tuscaloosa DY-HR TOWN	=== 66 64 64 64 64 68 73	=== 64 64 64 62 62 64 66 DEW	93 100 100 93 93 87 79 HUM	=== 66 64 64 62 66 76 FLK ===	N 0 N 0 N 0 N 0 N 0 N 5 N 5 NE 5 WIND GST	29.91 29.90 29.90 29.95 29.96 PRSSR	=== 5 4 5 5 5 6 7 VSB	BR BR VCFG BR BR BR	SKC SKC SKC SKC SKC SKC SKC SKC CLOUD COVER
12-08A Tuscaloosa 12-09A Tuscaloosa 12-10A Tuscaloosa 12-11A Tuscaloosa 12-11P Tuscaloosa 12-01P Tuscaloosa 12-02P Tuscaloosa DY-HR TOWN ===== ===============================	=== 66 64 64 64 64 68 73 TMP === 64	=== 64 64 64 62 62 64 66 DEW === 62	=== 93 100 100 93 93 87 79 HUM === 93	=== 66 64 64 62 66 76 FLK === 64	N 0 N 0 N 0 N 0 N 0 N 5 N 5 NE 5 WIND GST	29.91 29.90 29.90 29.95 29.96 PRSSR ===== 29.92	=== 5 4 5 5 5 6 7 VSB === 8	BR BR VCFG BR BR BR	SKC
12-08A Tuscaloosa 12-09A Tuscaloosa 12-10A Tuscaloosa 12-11A Tuscaloosa 12-11P Tuscaloosa 12-01P Tuscaloosa 12-02P Tuscaloosa 12-02P Tuscaloosa DY-HR TOWN ====== ==============================	=== 66 64 64 64 64 68 73 TMP === 64 62	=== 64 64 62 62 64 66 DEW === 62 60	=== 93 100 100 93 93 87 79 HUM === 93 93	=== 66 64 64 62 66 76 FLK === 64 62	N 0 N 0 N 0 N 0 N 0 N 5 N 5 N 5 NE 5 WIND GST ====== N 0 N 0	29.91 29.90 29.90 29.95 29.96 PRSSR ==== 29.92 29.92	=== 5 4 5 5 5 6 7 VSB === 8	BR BR VCFG BR BR BR	SKC
12-08A Tuscaloosa 12-09A Tuscaloosa 12-10A Tuscaloosa 12-11A Tuscaloosa 12-11P Tuscaloosa 12-01P Tuscaloosa 12-02P Tuscaloosa 12-02P Tuscaloosa 12-02P Tuscaloosa 12-02P Birmingham 12-09A Birmingham 12-10A Birmingham	=== 66 64 64 64 68 73 TMP === 64 62 62	=== 64 64 62 62 64 66 DEW === 62 60 60	=== 93 100 100 93 93 87 79 HUM === 93 93 93	=== 66 64 64 62 66 76 FLK === 64 62 62	N 0 N 0 N 0 N 0 N 5 N 5 N 5 NE 5 WIND GST ====== N 0 N 0 N 0	29.91 29.90 29.90 29.95 29.96 PRSSR ==== 29.92 29.92	=== 5 4 5 5 5 6 7 VSB === 8 7	BR BR VCFG BR BR BR	SKC
12-08A Tuscaloosa 12-09A Tuscaloosa 12-10A Tuscaloosa 12-11A Tuscaloosa 12-11P Tuscaloosa 12-01P Tuscaloosa 12-02P Tuscaloosa 12-02P Tuscaloosa 12-02P Birmingham 12-09A Birmingham 12-10A Birmingham 12-11A Birmingham	=== 66 64 64 64 68 73 TMP === 64 62 62 62	=== 64 64 62 62 64 66 DEW === 62 60 60 62	=== 93 100 100 93 93 87 79 HUM === 93 93 100	=== 66 64 64 62 66 76 FLK === 64 62 62 62	N 0 N 0 N 0 N 0 N 5 N 5 NE 5 WIND GST ====== N 0 N 0 N 0 N 0	PRSSR ==== 29.91 29.90 29.95 29.96 PRSSR ==== 29.92 29.92 29.92	=== 5 4 5 5 6 7 VSB === 8 7 7	BR BR VCFG BR BR BR BR BR	SKC
12-08A Tuscaloosa 12-09A Tuscaloosa 12-10A Tuscaloosa 12-11A Tuscaloosa 12-11P Tuscaloosa 12-01P Tuscaloosa 12-02P Tuscaloosa 12-02P Tuscaloosa DY-HR TOWN ===== ===============================	=== 66 64 64 64 68 73 TMP === 64 62 62 62 62	=== 64 64 62 62 64 66 DEW === 62 60 60 62 60	=== 93 100 100 93 93 87 79 HUM === 93 93 100 93	=== 66 64 64 62 66 76 FLK === 64 62 62 62 62	N 0 N 0 N 0 N 0 N 5 N 5 N 5 NE 5 WIND GST ====== N 0 N 0 N 0 N 0 N 0 N 0 NE 3	29.91 29.90 29.90 29.95 29.96 PRSSR ==== 29.92 29.92 29.92 29.92	=== 5 4 5 5 5 6 7 VSB === 8 7 7 5 4	BR	SKC
12-08A Tuscaloosa 12-09A Tuscaloosa 12-10A Tuscaloosa 12-11A Tuscaloosa 12-11P Tuscaloosa 12-01P Tuscaloosa 12-02P Tuscaloosa 12-02P Tuscaloosa 12-02P Tuscaloosa DY-HR TOWN ===== ===============================	=== 66 64 64 64 68 73 TMP === 64 62 62 62 62 62 66	=== 64 64 62 62 64 66 DEW === 62 60 60 64	=== 93 100 100 93 93 87 79 HUM === 93 93 100 93 93	=== 66 64 64 62 66 76 FLK === 64 62 62 62 66	N 0 N 0 N 0 N 0 N 5 N 5 N 5 NE 5 WIND GST ====== N 0 N 0 N 0 N 0 N 0 N 0 N 0 N 0 N 0 N 0	PRSSR ==== 29.92 29.92 29.94 29.95 29.96	=== 5 4 5 5 5 6 7 VSB === 8 7 7 5 4 4	BR B	SKC
12-08A Tuscaloosa 12-09A Tuscaloosa 12-10A Tuscaloosa 12-11A Tuscaloosa 12-11P Tuscaloosa 12-01P Tuscaloosa 12-02P Tuscaloosa 12-02P Tuscaloosa DY-HR TOWN ===== ===============================	=== 66 64 64 64 68 73 TMP === 64 62 62 62 62	=== 64 64 62 62 64 66 DEW === 62 60 60 62 60	=== 93 100 100 93 93 87 79 HUM === 93 93 100 93	=== 66 64 64 62 66 76 FLK === 64 62 62 62 62	N 0 N 0 N 0 N 0 N 5 N 5 N 5 NE 5 WIND GST ====== N 0 N 0 N 0 N 0 N 0 N 0 N 0 N 0 N 0 N 0	29.91 29.90 29.90 29.95 29.96 PRSSR ==== 29.92 29.92 29.92 29.92	=== 5 4 5 5 5 6 7 VSB === 8 7 7 5 4	BR	SKC

DY-HR	TOWN	TMP	DEW	HUM	FLK	WIND	GST	PRSSR	VSBLY	-WX	CLOUD	COVER
			===	===		====					======	======
	Anniston	64	64	100	64		0	29.90			SKC	
12-08A^	Anniston	SLP:		08422	2 00	OOOKI	1/851	I FG V	100T T	8/18	A2991 F	RMK
12 007	Anniston	SБР.	64	100	64	NT	^	20 01	0 15	a	1 7777	
	Anniston	64	64	100	64		0	29.91 29.91	0.1F 0.1F		1 VV 1 VV	
	Anniston	64	64	100	64		0	29.91			1 VV	
	Anniston	62	62	100	62		0	29.91			1 VV	
	Anniston	64	64	100	64		0	29.95			2 VV	
	Anniston						-				8 A2995	RMK
10 011 .		SLP				000111	±, 2 -				0 112333	
12-02P	Anniston	64		100	64	N	0	29.96	0.5F	G	4 VV	
12-02P*	Anniston	KANI	3 12:	14052	2 000	OOOKT	1 1/2	SM BR	SCT00	5 19,	/19 A299	5 RMK
		SLP:	141				•					
12-02P*	Anniston	KANI	3 12:	14112	3 000	000KT	4SM E	BR HZ B	FEW008	20/2	20 A 2996	RMK
		SLP:	144									
D	morn.	m>	D=	****			~~=	DD ~			GT 0	001
DY-HR	TOWN		DEW	HUM				PRSSR				
		===	===	===	===	====	====	=====	=====	=== :		======
	Centreville											
	Centreville Centreville											
	Centreville											
	Centreville											
	Centreville											
	Centreville											
12 021	CCITCLCATITE		3									
DY-HR	TOWN	TMP	DEW	HUM	FLK	WIND	GST	PRSSR	VSBLY	-WX	CLOUD	COVER
======	========	===	===	===	===	====	====	=====	=====	=== :	======	======
	Maxwell AFB	71	68	90			2	29.87	7		SKC	
	Maxwell AFB	69	68	97	69		2	29.87	7		SKC	
	Maxwell AFB	69	66	90	69		1	29.88	7		SKC	
	Maxwell AFB	68	64	87	68		3	29.89	6 B		SKC	
	Maxwell AFB	68	66	93	68		0	29.90	4 B		SKC	
	Maxwell AFB	71	66	84	69	VR	5	29.91	5 B	R	SKC	
12-02P*I	Maxwell AFB											
DY-HR	TOWN	тмъ	DEM	шттм	א. דיז	WIND	GST	PRSSR	VSRI.V	-WY	CLOUD	COVER
	=========										======	
	Montgomery	69	66	90	69		0	29.88			CLR	
	Montgomery	66	66	100	66		0	29.88			CLR	
	Montgomery	64	64	100	64		0	29.88			CLR	
	Montgomery	KMGI	1 120	09592	3 000	OOOKT	1 3/4			8/18	A2988 R	MK
	_	AO2										
12-10A*I	Montgomery	KMGI	1 12	10272	220	003KT	2 1/2	SM BR	SCT00	1 18,	/18 A298	9 RMK
		A02										
	Montgomery	66		100	66			29.89			1 VV	2 2
12-11A*I	Montgomery						2 1/2	SM BR	BKN00	1 18,	/18 A298	9 RMK
				1/25			2011	D D ****		/10 -	***************************************	
	Montgomery										A2990 RM	
	Montgomery							29.90			A2990 RM CLR	IN AUZ
	Montgomery	64 69	64 68	100 97			3 0	29.90			CLR	
	Montgomery Montgomery	69 73	68 69	97 87			3	29.92	5 H		CLR	
TZ-OZE I	Figure 3	, 5	0 9	0 /	, ,	A 1.C	<i>J</i>	20.00	<i>J</i> 11	_	CTIC	
DY-HR	TOWN	ТМР	DEW	МІЈН	FLK	WIND	GST	PRSSR	VSBLY	-WX	CLOUD	COVER
	======================================										======	
12-08A*												
	4											

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12-09A*Troy
12-10A*Troy
12-11A*Troy
                   64 62 93 64 SW 1 29.90 4 BR
12-12P Troy
                                                                     SKC
12-01P Troy
                   69 66 90 69 W
                                          2
                                                29.91 5 BR
                                                                     SKC
12-02P Troy
                75 66
                            74 78 N
                                           3
                                                29.91 7
                                                                     SKC
          TOWN TMP DEW HUM FLK WIND GST PRSSR VSBLY-WX CLOUD COVER
DY-HR
12-08A Mobile Brkly 71 69 93 71 NW 4 29.87 4 BR CLR 12-09A Mobile Brkly 71 62 73 69 NW 6 29.87 4 HZ CLR 12-10A Mobile Brkly 71 69 93 69 NW 6 29.88 4 BR CLR 12-11A Mobile Brkly 69 68 97 66 NW 6 29.89 4 BR CLR
12-11A*Mobile Brkly KBFM 121144Z 32003KT 2 1/2SM BR CLR 21/19 A2989 RMK
                     A02
12-12P Mobile Brkly 71 69 93
                                   71 N
                                         0
                                                 29.90 2.5BR
                                                                     CLR
12-01P Mobile Brkly 75 71 87 78 N
12-01P Mobile Brkly 75 71 87 78 N 6 29.91 2.5BR 12-02P Mobile Brkly 78 71 79 82 VR 3 29.91 2.5HZ
                                                                     CLR
                                                                     CLR
DY-HR
          TOWN
                     TMP DEW HUM FLK WIND GST PRSSR VSBLY-WX CLOUD COVER
12-08A Mobile Bates 71 68 90 71 N
                                          0 29.89 5 BR
                                                                     CLR
12-09A Mobile Bates 71 69 93 71 N 4 29.90 4 BR CLR 12-10A Mobile Bates 71 68 90 71 N 0 29.90 4 BR CLR 12-11A Mobile Bates 69 66 90 69 N 3 29.91 4 BR CLR 12-12P Mobile Bates 69 66 90 69 N 3 29.92 3 BR CLR
12-12P*Mobile Bates KMOB 121205Z 01004KT 2 1/2SM BR CLR 22/20 A2992 RMK
                     A02
12-12P*Mobile Bates KMOB 121213Z 02003KT 3SM BR CLR 22/20 A2992 RMK AO2
12-01P Mobile Bates 73 68 84 76 NE 5 29.93 4 HZ
12-02P Mobile Bates 77 68
                               74 80 NE
                                         5
                                                29.93 5
                                                           HZ
                                                                     CLR
                TMP DEW HUM FLK WIND GST PRSSR VSBLY-WX CLOUD COVER
DY-HR
          TOWN
12-08A Ozark FtRcke 69 66
                                           3 29.85 7
                             90 69 N
                                                                     SKC
12-09A Ozark FtRcke 69 69 100 69 N 3
                                                29.85 7
                                                                     SKC
12-10A Ozark FtRcke 69 69 100 69 N 2 29.86 7
12-11A Ozark FtRcke 69 68 97 69 N 3 29.87 7
12-12P Ozark FtRcke 69 68 97 69 N 3 29.89 5 BR
12-01P Ozark FtRcke 71 68 90 71 N 4 29.90 6 BR
12-02P Ozark FtRcke 77 66 69 79 N 5 29.90 6 HZ
                                                                     SKC
                                                                     SKC
                                                                     SKC
                                                                     SKC
                                                                     SKC
          TOWN
                     TMP DEW HUM FLK WIND GST PRSSR VSBLY-WX CLOUD COVER
12-08A Dothan 71 68 90 69 N 5 29.88 6 BR 12-09A Dothan 73 68 84 76 N 0 29.87 6 BR 12-10A Dothan 71 68 90 71 N 3 29.88 5 BR
12-09A Dothan 73 68 84 76 N
12-10A Dothan 71 68 90 71 N
12-11A Dothan 69 68 97 69 N
12-11A*Dothan KDHN 1211177 2000
                                                                 120 FEW
                                                                     SKC
                                                29.88 5 BR
                                                                     SKC
                                          3
                                                29.89 3 BR
                                                                 250 SCT
                    KDHN 121117Z 25005KT 2SM BR SCT250 21/19 A2990
                    69 68 97 67 NW 5 29.91 2 BR 250 SCT
12-12P Dothan
12-01P*Dothan
12-02P Dothan
                     77 68
                               74
                                   80 NW
                                          4
                                                29.92 3
                                                           BR
                                                                     CLR
          TOWN TMP DEW HUM FLK WIND GST PRSSR VSBLY-WX CLOUD COVER
29.89 7
12-08A Auburn 66 62 87 64 N 5
                                                                     CLR
12-09A Auburn 66 62 87 64 N 5
12-10A Auburn 64 62 93 64 N 3
12-11A Auburn 64 62 93 64 N 4
12-12P Auburn 66 62 87 63 NE 6
                                                29.89 7
                                                ∠9.89 7
29.90 7
                                                                     CLR
                                                                     CLR
                                                29.91 3.5
                                                                     CLR
                                                       7
                                                 29.92
                                                                     CLR
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